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# Development of inactive analogues for Fukushima nuclear debris: an initial assessment of corrosion behaviour

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# Context



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- ✓ On March 2011 at the Fukushima Daiichi NPP:
  - Loss of coolant accident
  - Partial meltdown of boiling water reactor Units 1 to 3
    - ↳ Increase of the temperature in the reactors up to 2000°C
    - ↳ Melting & reaction of  $UO_2$  with zircaloy fuel cladding



$U_{1-x}Zr_xO_2$   
**solid solution**

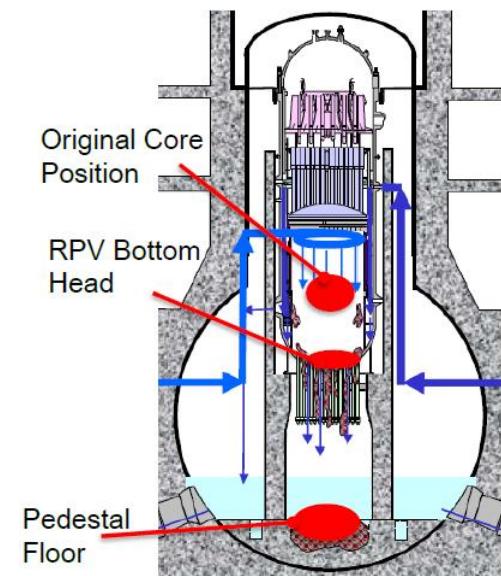
*Nuclear Fuel Debris (NFD)*



**NFD + Concrete  
+ Stainless steel**

*Corium*

- ✓ Cooling NFD and corium by water injection since the accident
    - Seawater
    - Fukushima NPP groundwater
    - Filtered water
- ↳ Temperature reduced < 100°C



# Objectives



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Need for an **understanding of their behaviour** in contact with solutions relevant to Fukushima molten core cooling

Synthesise **realistic simulant of NFD and Corium**

- ✓ Syntheses and Characterisation
  - ⇒  $Ce_{1-x}Zr_xO_2$  solid solutions ( $0 < x < 0.9$ )
  - ⇒ Corium
- ✓ Degradation of realistic simulant fuel debris and corium
  - ⇒ Different dissolution media (nitric acid, groundwater, filtered water)
  - ⇒ One temperature ( $60^\circ C$ )

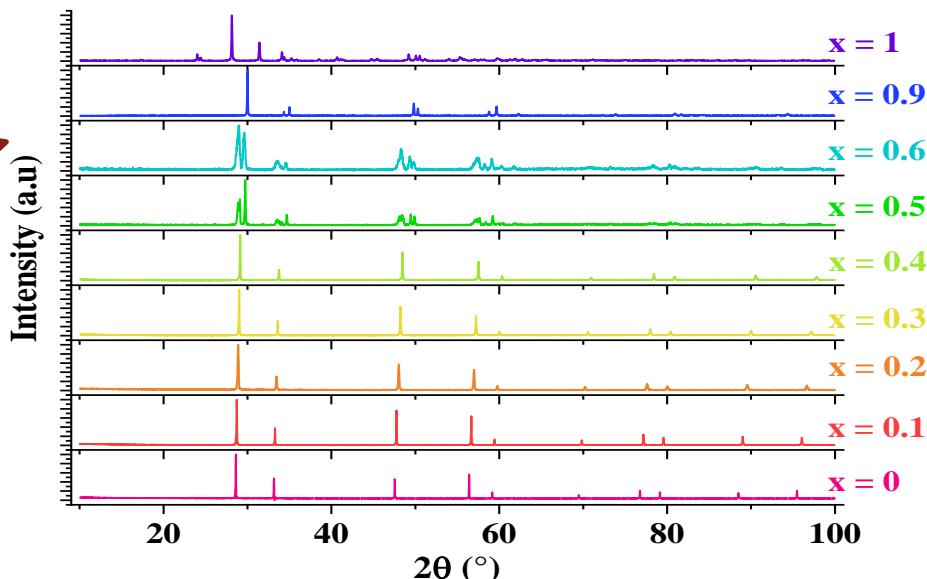
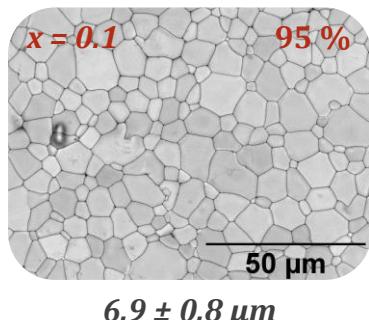
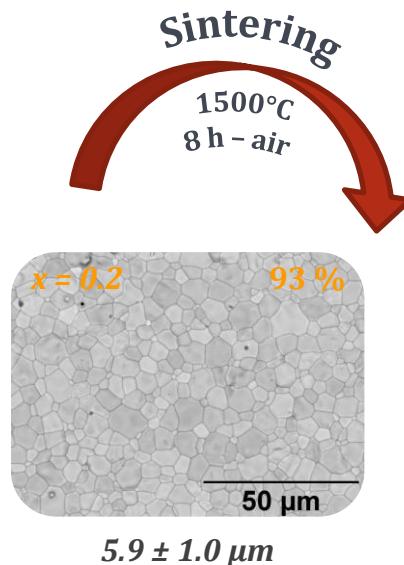
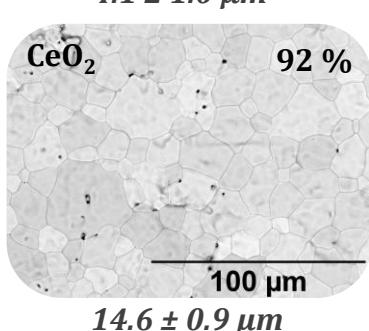
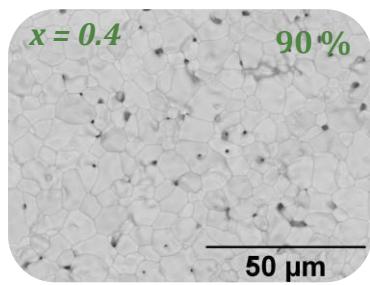
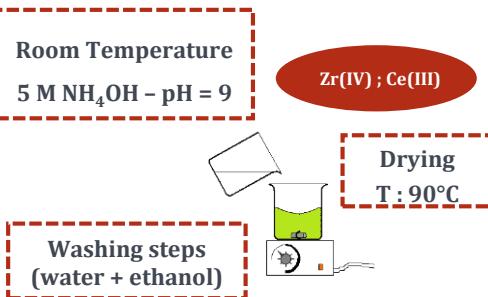


# Synthesis of $\text{Ce}_{(1-x)}\text{Zr}_x\text{O}_2$



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Composition	Lattice parameter ( $\text{\AA}$ )	Literature
$\text{CeO}_2$	$5.4041 \pm 0.0021$	5.453(7)
$\text{Ce}_{0.90}\text{Zr}_{0.10}\text{O}_{2\pm y}$	$5.3813 \pm 0.0013$	-
$\text{Ce}_{0.80}\text{Zr}_{0.20}\text{O}_{2+y}$	$5.3531 \pm 0.0016$	-
$\text{Ce}_{0.75}\text{Zr}_{0.25}\text{O}_2$	-	5.3621
$\text{Ce}_{0.60}\text{Zr}_{0.40}\text{O}_{2\pm y}$	$5.3085 \pm 0.0011$	-

✓ Incorporation of Zr into fluorite structure

→ Lattice contraction due to the incorporation of smaller size  $\text{Zr}^{4+}$  in  $\text{CeO}_2$

$\text{Ce}^{4+}$  (VIII): 0.97  $\text{\AA}$

$\text{Zr}^{4+}$  (VIII): 0.84  $\text{\AA}$

# Dissolution test: Methodology



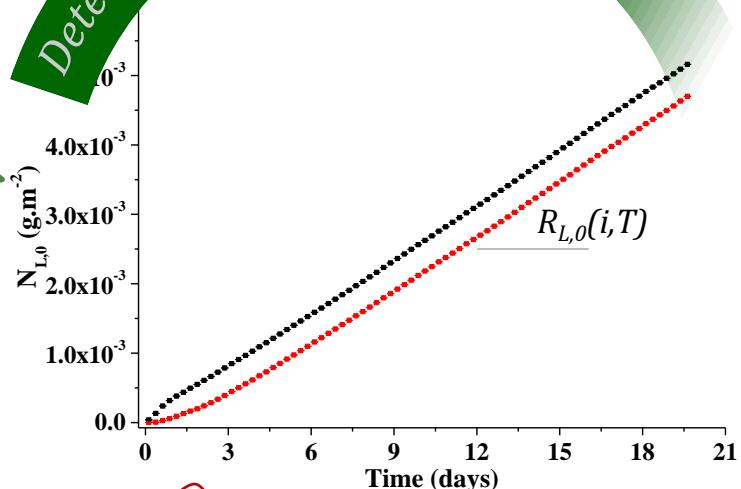
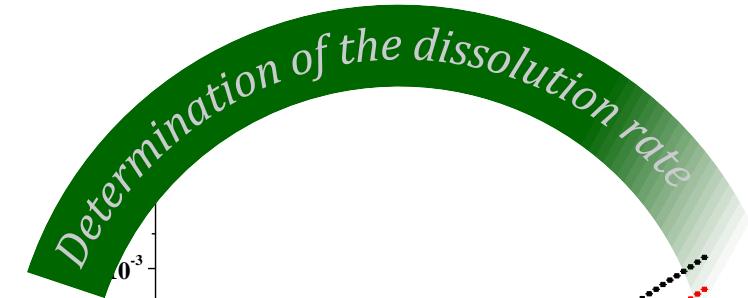
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*Close to  
equilibrium*



$$R_L(i, T) = k \times e^{-E_a/RT} \times g(I) \times \prod_i (a_i)^{n_i} \times f(\Delta_R G)$$



$$R_{L,0}(i, T) = \frac{dN_L(i)}{dt} = \frac{1}{f_i} \times \frac{d}{dt} \left( \frac{C_i \times V}{S} \right)$$

Amount of ( $E_i$ ) in solution ( $g.L^{-1}$ )  
Effective surface area ( $m^2$ )  
Mass ratio of ( $E_i$ ) in the solid

$R_L(i) \approx R_L(j)$  Congruent dissolution

$R_L(i) \neq R_L(j)$  Incongruent dissolution

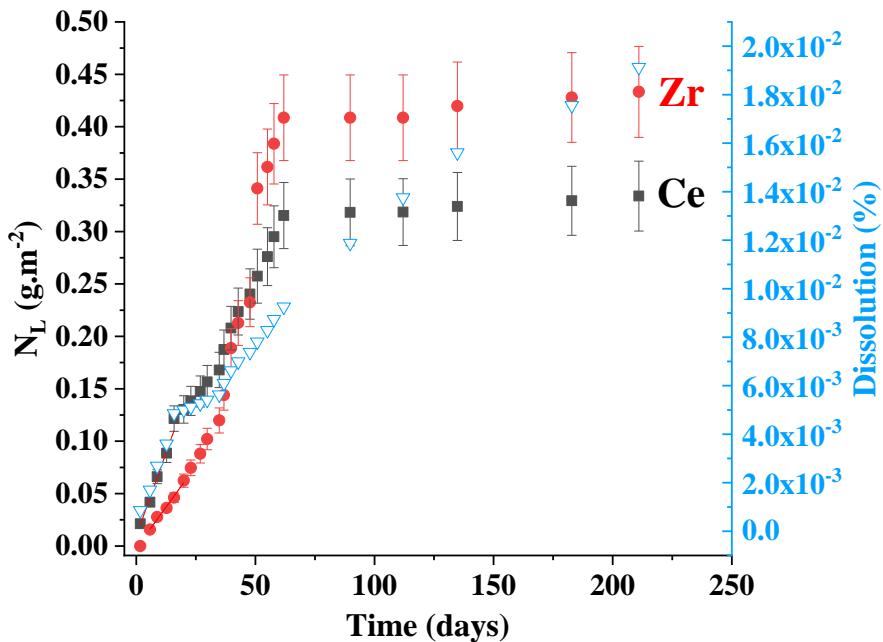
# Dissolution test: 9 M HNO<sub>3</sub> – 60°C



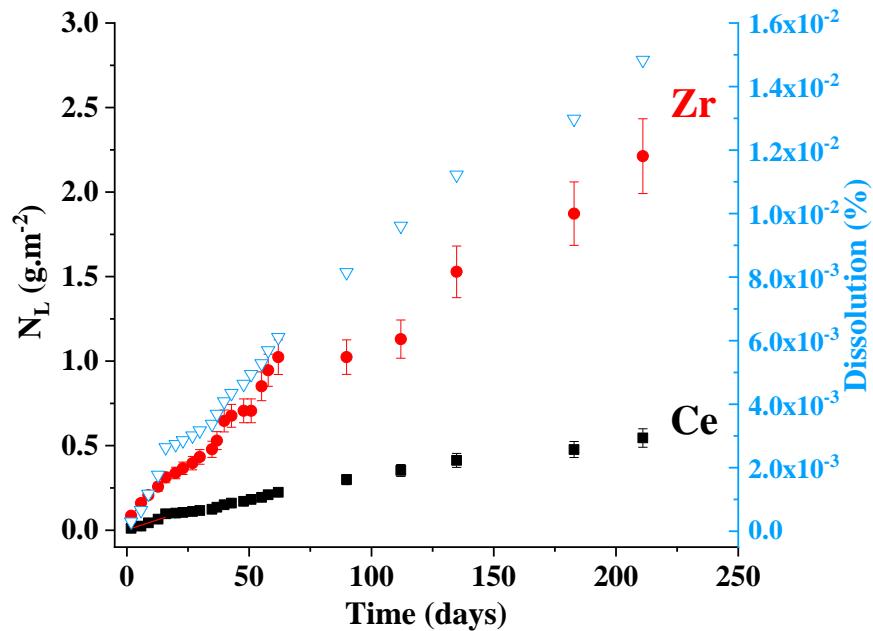
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✓ Ce<sub>0.6</sub>Zr<sub>0.4</sub>O<sub>2</sub>



✓ Ce<sub>0.8</sub>Zr<sub>0.2</sub>O<sub>2</sub>



$$R_{L,0}(\text{Ce}) = (6.34 \pm 0.44) \times 10^{-3} \text{ g.m}^{-2}.\text{d}^{-1}$$

$$R_{L,0}(\text{Zr}) = (3.14 \pm 0.19) \times 10^{-3} \text{ g.m}^{-2}.\text{d}^{-1}$$

$$R_{L,0}(\text{Ce}) = (2.63 \pm 0.16) \times 10^{-3} \text{ g.m}^{-2}.\text{d}^{-1}$$

$$R_{L,0}(\text{Zr}) = (1.38 \pm 0.09) \times 10^{-2} \text{ g.m}^{-2}.\text{d}^{-1}$$

⇒ Slight increase of the  $R_{L,0}$  when increasing the amount of Zr in the oxide

- ↳ Potential presence of Ce<sup>3+</sup> (sintering in air)
- ↳ Presence of oxygen vacancies

Increase of the structural defects

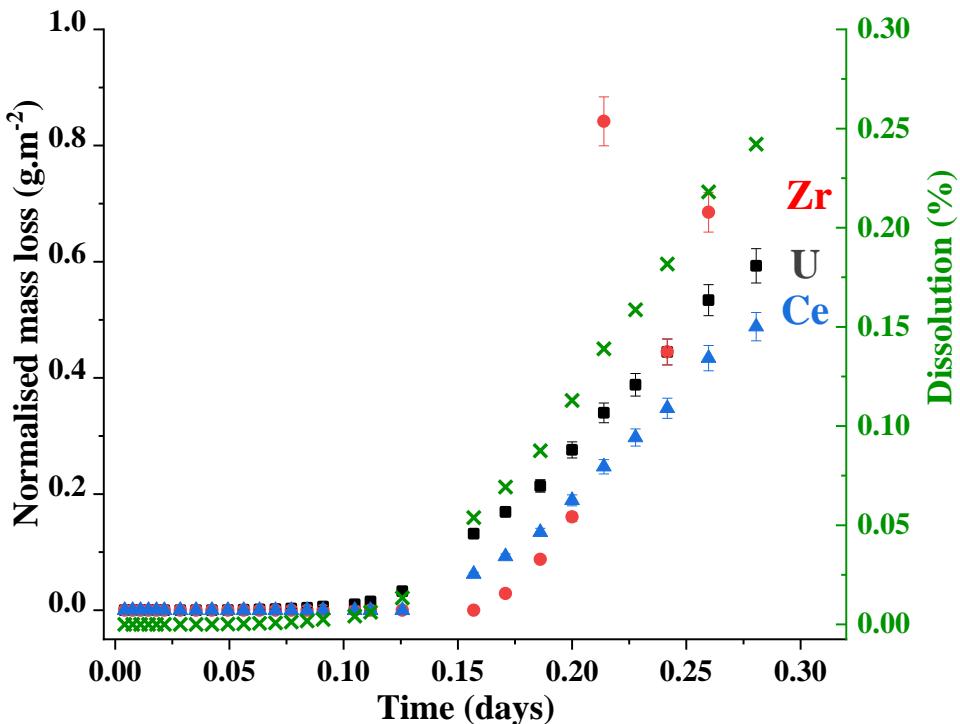
# Dissolution test: 2 M HNO<sub>3</sub> – 60°C

✓ U<sub>0.9</sub>Ce<sub>0.05</sub>Zr<sub>0.05</sub>O<sub>2</sub>

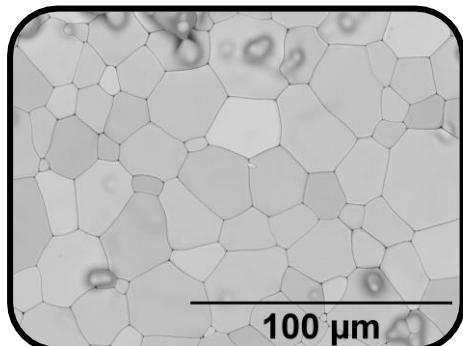


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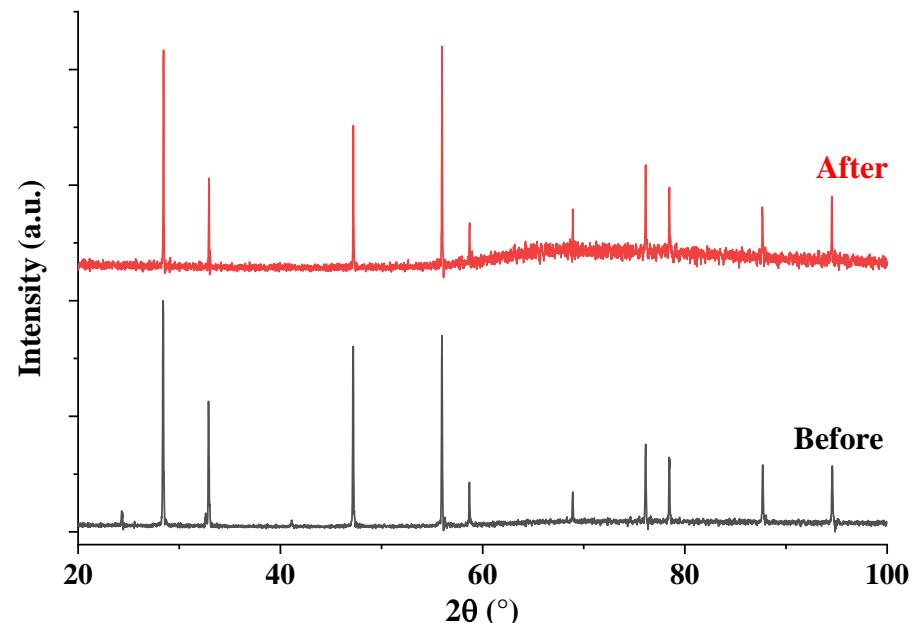
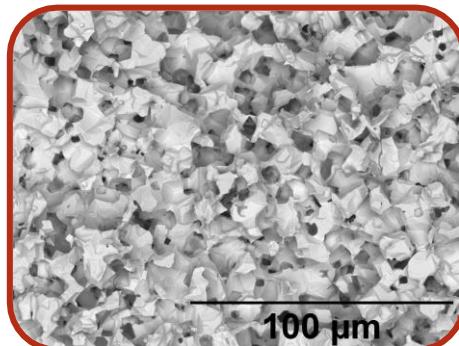
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*Before*



*After*



$$R_L(U) = 3.726 \pm 0.131 \text{ g.m}^{-2}.\text{d}^{-1}$$

$$R_L(Ce) = 3.297 \pm 0.163 \text{ g.m}^{-2}.\text{d}^{-1}$$

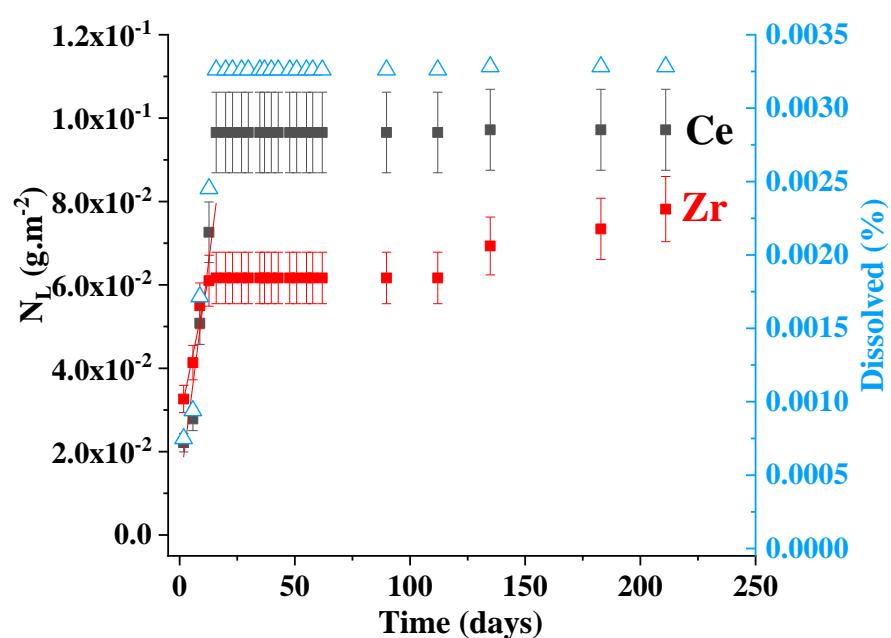
→ Decrease of the  $R_L$  in presence of Zr in the oxide

$$\textcolor{red}{\leftarrow} R_L(U) = 22 \pm 2 \text{ g.m}^{-2}.\text{d}^{-1}^*$$

$$\textcolor{red}{\leftarrow} R_L(\text{Zr} - 90^\circ\text{C}) = 8.64 \times 10^{-4} \text{ g.m}^{-2}.\text{d}^{-1}^*$$

# Dissolution test: 19 mM NaCl & 1 mM NaHCO<sub>3</sub> - 60°C

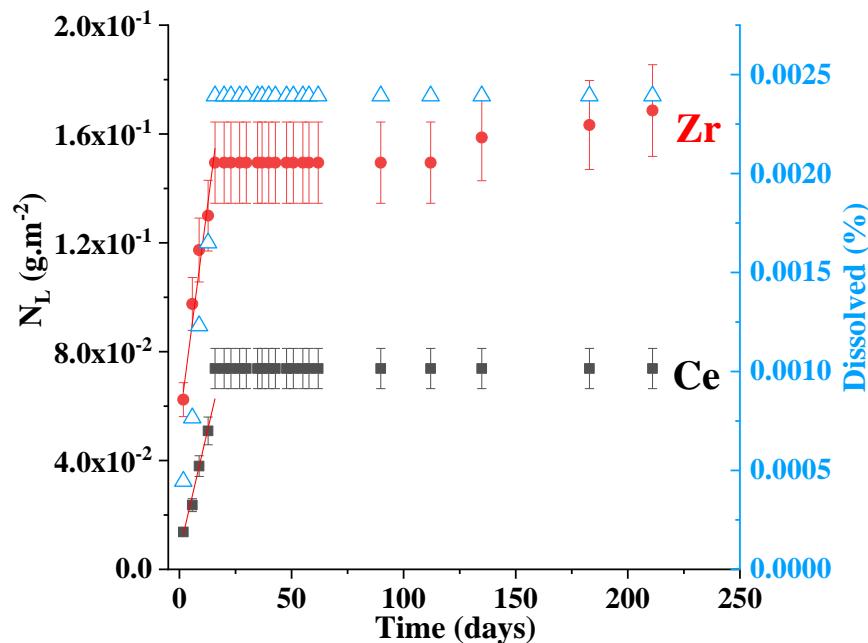
✓ Ce<sub>0.6</sub>Zr<sub>0.4</sub>O<sub>2</sub>



$$R_{L,0}(\text{Ce}) = (4.31 \pm 0.99) \times 10^{-3} \text{ g.m}^{-2} \cdot \text{d}^{-1}$$

$$R_{L,0}(\text{Zr}) = (2.71 \pm 0.33) \times 10^{-3} \text{ g.m}^{-2} \cdot \text{d}^{-1}$$

✓ Ce<sub>0.8</sub>Zr<sub>0.2</sub>O<sub>2</sub>



$$R_{L,0}(\text{Ce}) = (3.53 \pm 0.40) \times 10^{-3} \text{ g.m}^{-2} \cdot \text{d}^{-1}$$

$$R_{L,0}(\text{Zr}) = (6.34 \pm 0.61) \times 10^{-3} \text{ g.m}^{-2} \cdot \text{d}^{-1}$$

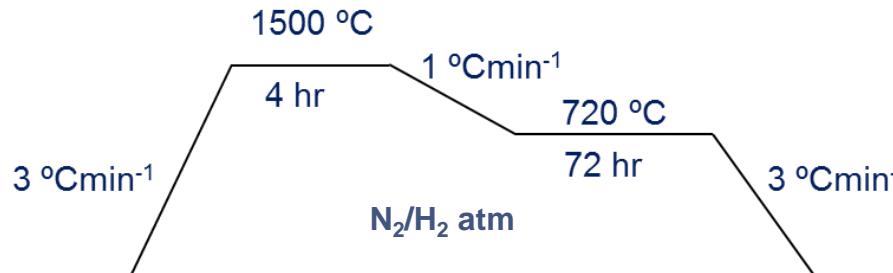
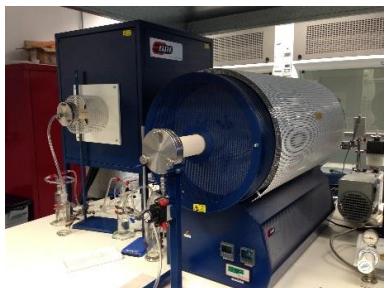
- Release of the elements at the beginning of the dissolution
- Observation of a plateau (no more dissolution ?): formation of Ce<sub>2</sub>(CO<sub>3</sub>)<sub>3</sub>·nH<sub>2</sub>O ?
- R<sub>L,0</sub> higher than in UHQ

# Synthesis of Simulant Fukushima Corium through thermal route

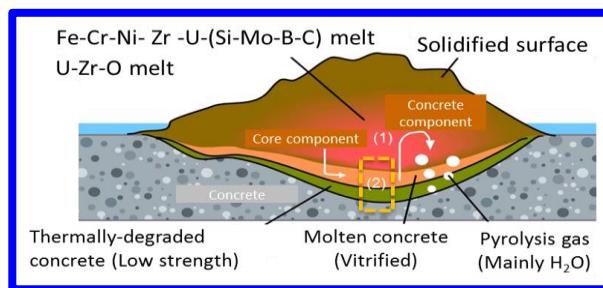
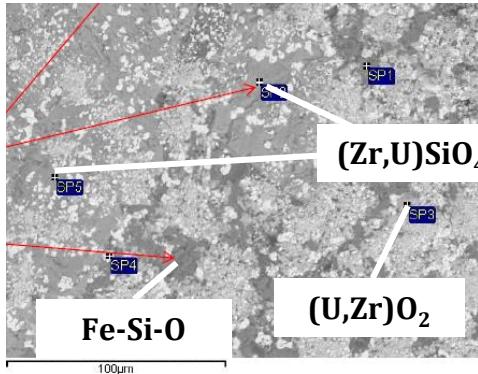


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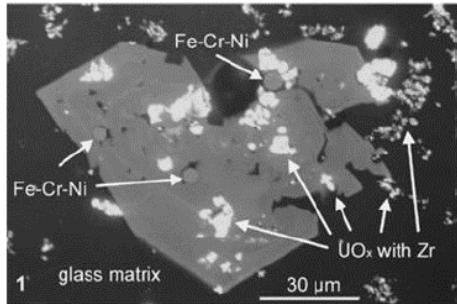
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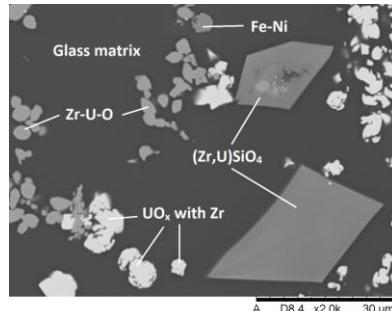
Fukushima – Vulcano MCCI samples



Chernobyl – LFCM



Simulant – LFCM



Component	C1 Wt.%	C2 %	C3 Wt.%
SiO <sub>2</sub>	43.6	43.6	43.6
CaO	8.85	8.85	8.85
ZrO <sub>2</sub>	<b>4.56</b>	<b>4.56</b>	<b>4.56</b>
Al <sub>2</sub> O <sub>3</sub>	10.78	10.78	10.78
Stainless Steel	2	2	2
Ce <sub>0.8</sub> Zr <sub>0.2</sub> O <sub>2</sub>	–	10.87	–
CeO <sub>2</sub>	10.87	–	–
Ce <sub>0.6</sub> Zr <sub>0.4</sub> O <sub>2</sub>	–	–	10.87

Tanabe, J. Nucl. Sci. Technol., 2011

Washiya, Management of Severely Damaged Spent Fuel and Corium conference, 2019

Anderson, Radiochim Acta, 1993

Clémence Gausse

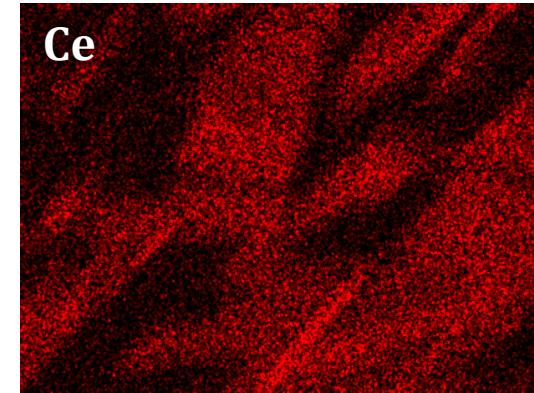
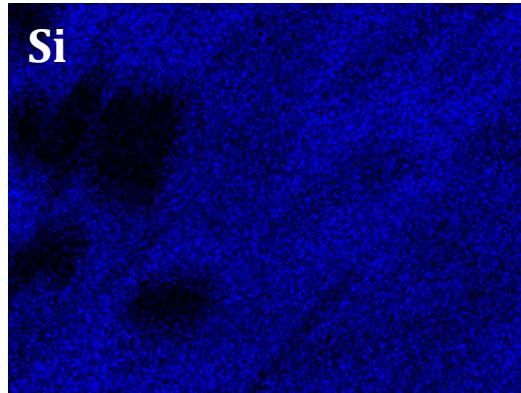
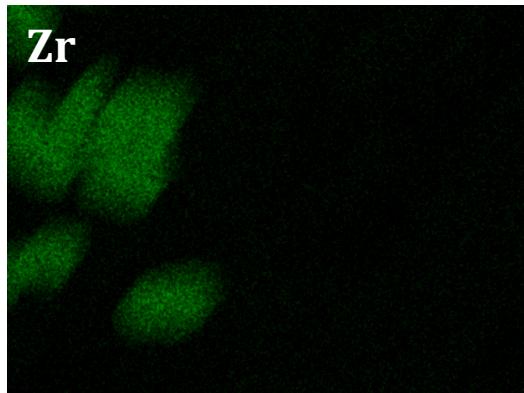
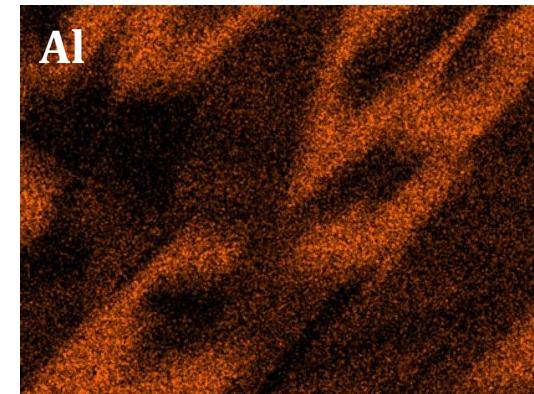
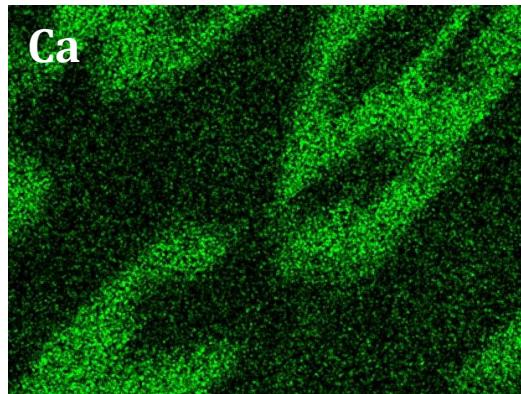
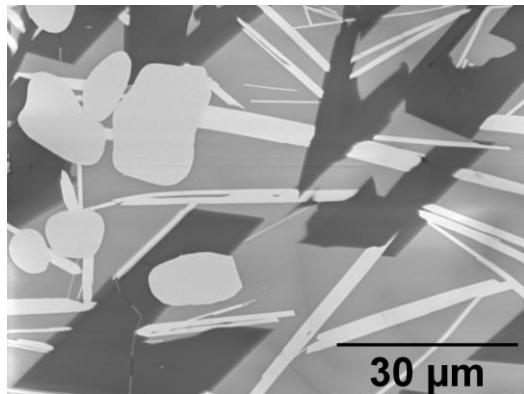
# Characterisation of Simulant Fukushima Corium



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✓ C1 – CeO<sub>2</sub>



- All 3 samples present a Ca and Al rich glassy phase
- Zr rich phase and Ce rich phase

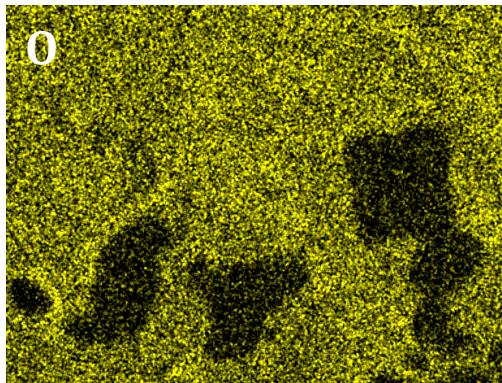
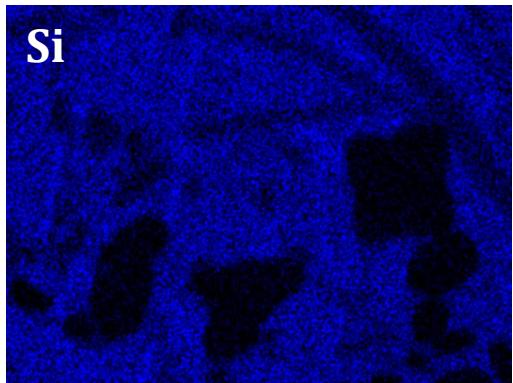
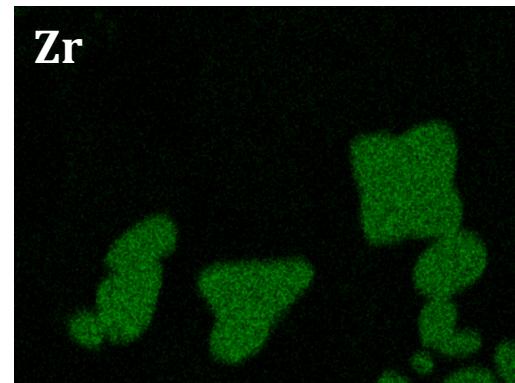
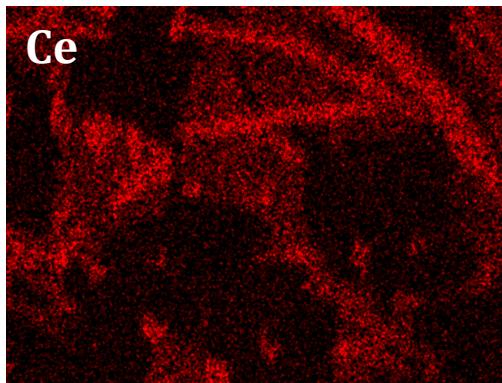
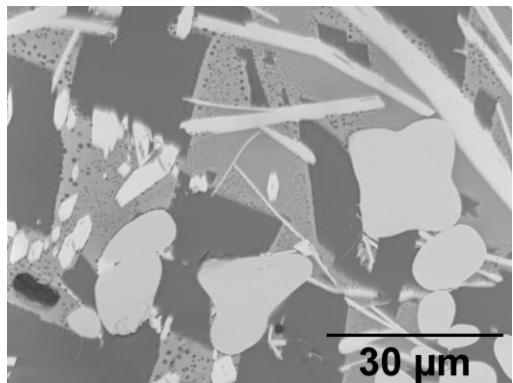
# Characterisation of Simulant Fukushima Corium



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✓ C2 – Ce<sub>0.8</sub>Zr<sub>0.2</sub>O<sub>2</sub>



- Ce rich phase : Ce<sub>2</sub>O<sub>3</sub> or CeO<sub>2</sub>
  - ↳ Reducing atmosphere process
- Si and Ce rich phase: part of Ce in a glass matrix
- Zr rich phase : Zr metal?

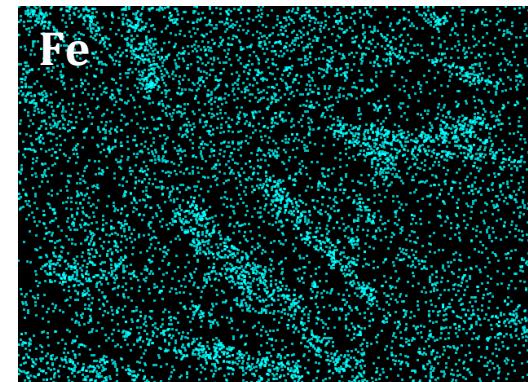
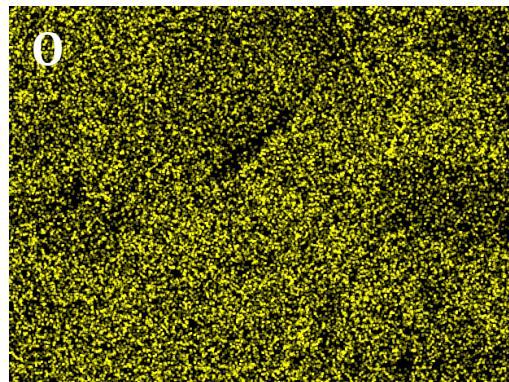
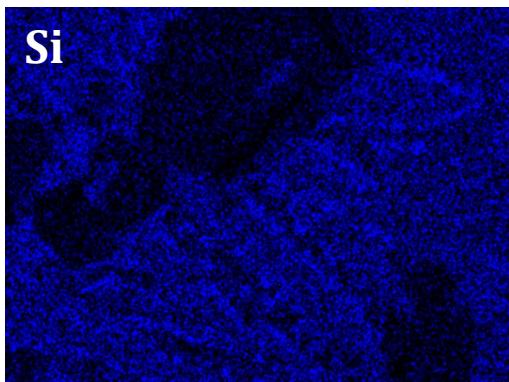
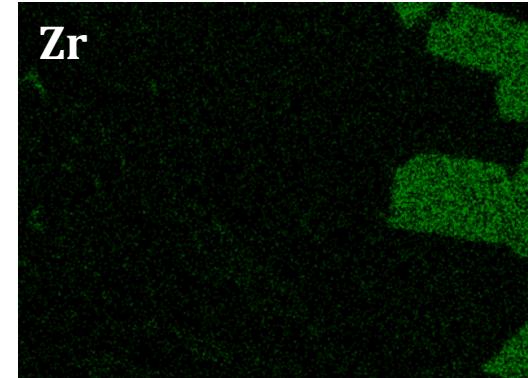
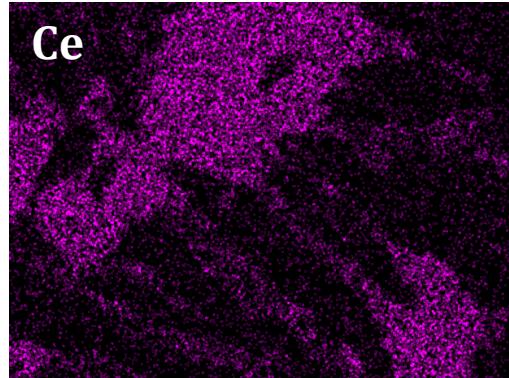
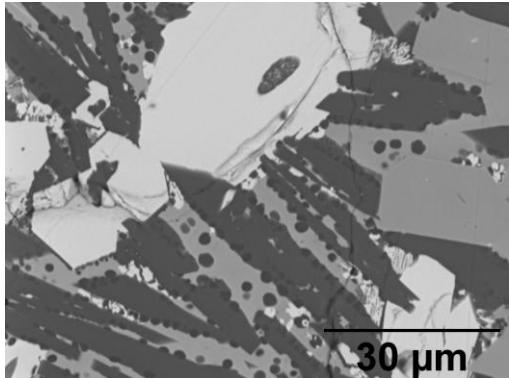
# Characterisation of Simulant Fukushima Corium



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✓ C3 – Ce<sub>0.6</sub>Zr<sub>0.4</sub>O<sub>2</sub>



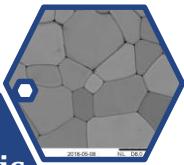
- Zr and Si rich phase: ZrSiO<sub>4</sub>
- Si and Fe rich phase
- Ce rich phase: CeO<sub>2</sub> or Ce<sub>2</sub>O<sub>3</sub>

# Conclusion and further work



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Synthesis

- Synthesis of  $\text{Ce}_{1-x}\text{Zr}_x\text{O}_2$  through wet chemistry routes
  - ↳ Incorporation into the fluorite  $\text{CeO}_2$  structure (40 mol.% Zr)
  - ↳ Incorporation of Zr into the fluorite  $\text{UO}_2$  structure up to 30 mol.%



Leaching

- No clear evidence of the Zr effect on the dissolution
  - ↳ Release of the Ce slightly higher with the incorporation of Zr
  - ↳ Inhibition of the dissolution of U in presence of Zr
- Difference observed between U and Ce might be due to the presence of  $\text{Ce}^{3+}$ 
  - ↳  $\text{Ce}^{3+}$  more mobile and soluble than  $\text{U}^{4+}$
- Strong refractory behavior of  $\text{Ce}_{1-x}\text{Zr}_x\text{O}_2$



Corium

- Similar morphology of the Fukushima corium
- Presence of  $\text{Ce}_2\text{O}_3$  due to reducing atmosphere treatment
- Presence of Zr(m)

Need for a Raman spectroscopy study of  $\text{Ce}_{1-x}\text{Zr}_x\text{O}_2$   
Further investigation on the Ce-analogue Fukushima corium



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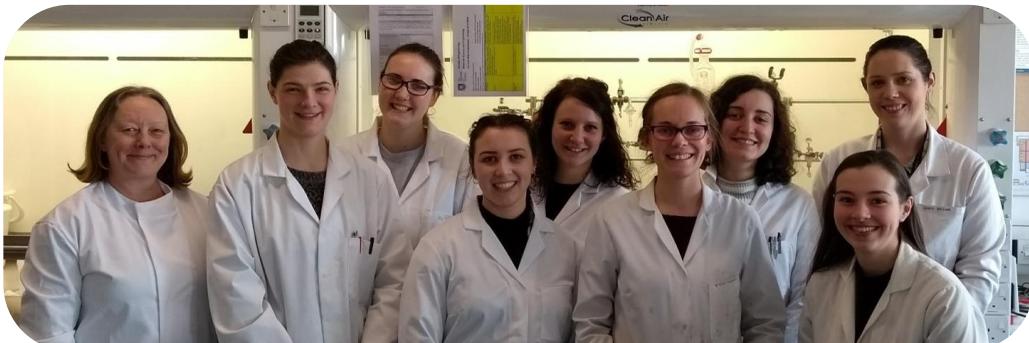
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# Thank you !



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